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# Silicon avalanche photodiode with photoresponse rise time less than 350 ps at wavelength 1064 nm

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The optical, electrical and dynamic characteristics of the developed silicon avalanche photodiode with an active area diameter of  $350\,\mu$ m were studied. It is shown that the developed avalanche photodiode has the following set of characteristics: external quantum output is 215 electrons/photon at a wavelength of 1064 nm, dark current is 0.77 nA, multiplication factor is 2353, rise time is less than 350 ps at a reverse bias voltage of 274 V.

Keywords: silicon, avalanche photodiode, near-infrared, lidar.

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Detectors operating in the near infrared range with a rise time below 1 ns have several applications in scientific, commercial, industrial, and aerospace instrumentation engineering. The spectral range around 1064 nm is one of the promising ones for such systems: first, laser emitters and photodetectors designed for these wavelengths are readily available; second, the level of interference from solar radiation here is several times lower than the corresponding level in the visible region. The determination of orbit altitude of navigation satellites with a laser ranging device (satellite laser ranging, SLR) [1,2] is one example of the applications mentioned above. Unfortunately, the distribution of detailed scientific and technical information on devices of this kind is restricted deliberately; it is also important that such detector parameters as area, capacitance, response time, and packaging type need to be optimized for a specific practical Silicon detectors are the optimum choice in the task. range in question, since detectors based on materials with a smaller band gap feature higher levels of excess noise [3]. Two types of detectors are practically available: avalanche detectors and single-photon ones. The latter devices are used at pulse repetition rates lower than 100 kHz and have a several orders of magnitude smaller area [4]. No commercial silicon avalanche photodiodes (APDs) designed for wavelength  $\lambda = 1064$  nm with a response time below 400 ps are currently produced in Russia. The aim of the present study is to examine the electrical, spectral, and dynamic characteristics of a silicon APD that was designed at the In Institute for operation at  $\lambda = 1064$  nm.

We have already reported [5] on the fabrication of a silicon APD with an active area diameter of  $1500 \,\mu$ m, an active area thickness of  $\sim 100 \,\mu$ m, and a rise time of 1500 ps at a wavelength of 1060 nm. In the present study, which was aimed at reducing the photoresponse rise time,

a silicon APD with an active area diameter of  $350\,\mu\text{m}$ and an active area thickness of  $\sim 20\,\mu\text{m}$  was designed, fabricated, and examined. The structure of this reachthrough APD is of a front-illuminated type (Fig. 1, *a*). The term "reach-through" implies that the APD operates under total substrate depletion. A photographic image of the examined APD is shown in Fig. 1, *b*.

Its characteristics were measured in a laboratory environment at a temperature of 22-23°C. The absolute values of responsivity (**R**) and external quantum yield (EQY) of the APD were determined in accordance with the procedure outlined in [5]. Spectral dependences of **R** and EQY at a reverse bias voltage of 230 V are presented in Fig. 2, *a*. A Keithley 6487 picoammeter with a built-in power supply was used to examine the reverse branch of the current– voltage curve. The capacitance–voltage curve was measured with Keithley 2400. The results are presented in Fig. 2, *b*.

Subsequent measurements were performed for  $\lambda = 1064$  nm. The dependence of EQY on the reverse bias voltage (Fig. 3, *a*) was determined in DC measurements with the use of a setup including a spectrophotometer (see [3] for details). The dependence of the APD rise time on the reverse voltage (Fig. 3, *a*) was determined using a digital oscilloscope, a picosecond laser diode [6], the power supply of a Keithley 6487 picoammeter, and a transimpedance amplifier with a bandwidth of 2.8 GHz and a gain of 1500 V/A. The inset of Fig. 3, *a* presents an oscilloscope record of the APD response to a laser pulse at a reverse bias voltage of 240 V. The response of the calibrated photodiode with a response time of 20 ps to a laser pulse is shown in Fig. 3, *b*.

Let us examine the spectral dependence of EQY in Fig. 2, *a* (curve 1). It follows from the presented data that the APD EQY for  $\lambda = 800$  nm is at the level of 25



**Figure 1.** a — APD structure. 1 — Metallic contacts, 2 — silicon dioxide, 3 — silicon  $n^{++}$  layer, 4 — p-type avalanche multiplication region, 5 — p-type silicon, and 6 — silicon  $p^{++}$  layer. b — Photographic image of the APD crystal.



**Figure 2.** APD parameters. a — Spectral dependences of the external quantum yield (1) and the responsivity (2). b — Dependences of the dark current (1) and the capacitance (2) on the reverse bias voltage.

electrons/photon at a reverse bias voltage of 230 V. Since the APD active area has no anti-reflective coating, it is assumed that reflection losses are at the level of ~ 33%, which is set by the optical properties of silicon [7]. Losses in the  $n^{++}$ - layer may be neglected, since its thickness is ~ 0.5  $\mu$ m, while the absorption depth of radiation with  $\lambda = 800$  nm in silicon is ~ 10  $\mu$ m. We assume that 67% of incident radiation with this wavelength are absorbed completely in the active area of the APD with a thickness of 20  $\mu$ m. The following expression is used to determine the APD multiplication factor at a reverse bias voltage of 230 V ( $M_{230}$ ):

$$M_{230} = \mathrm{EQY}(800)_{230}/0.67,\tag{1}$$

where EQY<sub>230</sub> is the external quantum yield of the APD for  $\lambda = 800 \text{ nm}$  at a reverse bias voltage of 230 V and 0.67 is a coefficient needed to factor in the reflection losses and the assumed complete absorption of radiation with  $\lambda = 800 \text{ nm}$  in the APD active area. The  $M_{230}$  value is then  $\sim 37$ .

The data for dependence 1 in Fig. 3, a and the following expression are used to determine the APD multiplication

factor at a reverse bias voltage of  $274 \text{ V} (M_{274})$ :

$$M_{274} = M_{230} EQY(1064)_{274} / EQY(1064)_{230}, \qquad (2)$$

where EQY(1064)<sub>274</sub> is the external quantum yield of the APD for  $\lambda = 1064$  nm at a reverse bias voltage of 274 V (215 electrons/photon) and EQY(1064)<sub>230</sub> is the external quantum yield of the APD for  $\lambda = 1064$  nm at a reverse bias voltage of 230 V (3.38 electrons/photon). Thus, the value of  $M_{274}$  for the examined APD is ~ 2353.

Comparing the characteristics of the proposed APD with the parameters of similar commercially available diodes produced in Russia, one should consider the SPD-031P photodiode [8] with an active area  $500 \,\mu\text{m}$  in diameter, the sensitivity maximum around 830 nm, a capacitance of 1 pF, and a rise time of 500 ps (the radiation wavelength is not indicated). Compared to SPD-031P, the presented APD has a two times smaller active area and a three times higher capacitance, but its rise time at  $\lambda = 1064 \,\text{nm}$  is 1.4 times shorter. This is likely attributable to the fact that this APD has a thinner active area than SPD-031P. Unfortunately, a



Figure 3. a — Dependences of the external quantum yield (1) and the rise time (2) of the APD on the reverse bias voltage. b — Response of the calibrated photodiode to a laser pulse.

fully correct comparison cannot be made, since the data for SPD-031P at  $\lambda = 1064$  nm are lacking.

Thus, the results of examination of optical, electrical, and dynamic characteristics of the designed silicon APD with an active area  $350\,\mu$ m in diameter were presented. It was demonstrated that this APD has the following set of characteristics at a temperature of  $22-23^{\circ}$ C and a reverse bias voltage of 260-274 V: an external quantum yield of 12-215 electrons/photon for  $\lambda = 1064$  nm, a dark current of 0.34-0.77 nA, a capacitance of 3 pF, and a rise time below 350 ps. It follows that the presented APD may be regarded as a promising candidate for LIDAR applications (e.g., in the SLR region [1,2]).

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### **Conflict of interest**

The authors declare that they have no conflict of interest.

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